

HIGH TEMPERATURE WEAR OF ADVANCED CERAMICS

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Introduction

It was initially hypothesized that advanced ceramics would exhibit favorable high temperature friction and wear properties because of their high hardness and low achievable surface roughness characteristics [1]. Further, localized asperity tip welding observed in metals does not occur in ceramics. More recent tribological studies of many nitride, carbide, oxide and composite ceramics, however, have revealed that ceramics often exhibit high friction and wear in non-lubricated, high temperature sliding contacts [2 to 5]. Table 1 summarizes measured friction and wear factor coefficients for a variety of ceramics from self mated ceramic pin-on-disk tests at temperatures from 25 to up to 1200 °C. Observed steady state friction coefficients range from about 0.5 to 1.0 or above. Wear factor coefficients are also very high and range from about 10^{-5} to 10^{-2} mm³/N-m. By comparison, oil lubricated steel sliding results in friction coefficients of 0.1 or less and wear factors less than 10^{-9} mm³/N-m.

Microscopic analyses of worn ceramic surfaces reveal two major modes of wear: brittle fracture and tribo-oxidative wear. High friction coefficients during sliding generate high tensile stresses in the wake of the contact area [6]. If sufficiently large flaws exist, cracks form, grow and ultimately lead to faceted wear debris formation (Figure 1). Brittle wear predominates at lower temperatures for all ceramics and at high temperatures brittle behavior is a common feature for oxide materials like alumina. Nitride and carbide containing ceramics sliding at high temperature in air form complex and often glassy oxide surface layers which are removed by the sliding counter-face revealing fresh, non-oxidized surfaces. These then oxidize resulting in an oxidative type wear process. The wear debris from these tests is often characterized by smeared oxide layers and sometimes even "rolled up" layered debris (Figure 2).

Ceramics possess useful thermal, physical and chemical properties and can be used provided their shortcomings are accommodated. For instance, oil lubricated silicon nitride is successful in fuel injectors and hybrid ball bearings. As research efforts progress, advanced ceramics will find ever increasing applications in engineering and technology.



Fig. 1 TEM photomicrograph of faceted wear debris following room temperature sliding of an Al₂O₃-SiC_w whisker reinforced ceramic composite [4].



Fig. 2 Ceramic wear debris formed from oxide layer removal on Al₂O₃-SiC_w disk specimen following 1200 °C sliding in air [4].

Table 1. Friction and wear summary for pin-on-disk sliding of ceramics

Pin /Disk Material, °C	Friction Coefficient	Average Wear Coefficient, mm ³ /N-m	Wear Mode,** ref. no.
Al ₂ O ₃ (25)	0.84	10 ⁻⁷	M (3)
Al ₂ O ₃ (1000)	0.50	10 ⁻⁷	M (3)
SiC (25)	0.75	10 ⁻⁷	M (3)
SiC (1000)	0.77	10 ⁻³	O (3)
Si ₃ N ₄ (25)	0.60	10 ⁻³	M (2)
Si ₃ N ₄ (1000)	0.70	10 ⁻²	O (2)
*Al ₂ O ₃ -SiC _w (25)	0.74	10 ⁻⁷	M (4)
Al ₂ O ₃ -SiC _w (1200)	0.58	10 ⁻⁶	MO (4)
ZrO ₂ (25)	0.68	10 ⁻⁴	M (5)
ZrO ₂ (800)	0.65	10 ⁻⁴	M (5)

*Al₂O₃-SiC_w is alumina with 25 volume percent silicon carbide whiskers added.

**M = microfracture, O = oxide-layer removal, MO = microfracture-oxidation

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